

## 60V 4-Switch Buck-Boost Controller with Bidirectional Mode

### DESCRIPTION

The VE8622 is a synchronous 4-switch buck-boost voltage/current regulator controller with bidirectional mode. The VE8622 can regulate output voltage, output current, or input current with input voltages above, below, or equal to the output voltage. The constant-frequency, current mode architecture allows its frequency to be adjusted or synchronized from 100kHz to 700kHz. No top FET refresh switching cycle is needed in buck or boost operation. With 60V input, 60V output capability and seamless transitions between operating regions, the VE8622 is ideal for voltage regulator, battery/super-capacitor charger applications in automotive, industrial, telecom, and even battery-powered systems.

The VE8622 can operate bidirectional mode with CV and CC control for both directions.

DIR pin is used to set direction and VE8622 can work in buck, boost and buck-boost mode for both directions. It can regulate input voltage, output voltage, forward current and reverse current.

The VE8622 provides input current monitor, output current monitor, and various status flags, such as C/10 charge termination and shorted output flag for both directions.

The VE8622 is available in TSSOP38-EP package. This package uses EPAD to improve thermal performance and noise immunity.

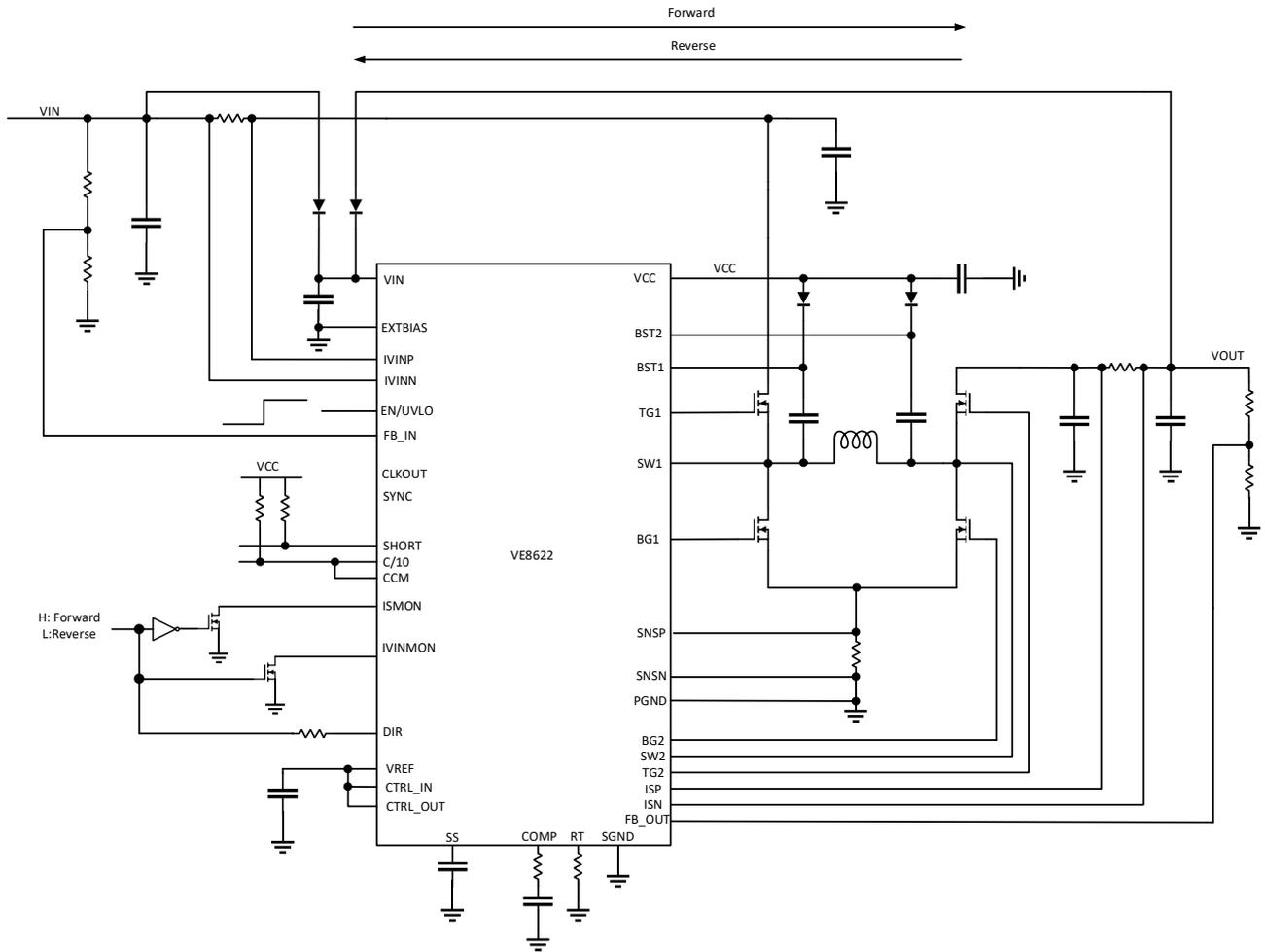
### FEATURES

- CV/CC control with bidirectional mode
- 4-Switch Single Inductor Architecture Allows VIN Above, Below or Equal to VOUT
- Synchronous Switching: Up to 98.5% Efficiency
- Wide VIN Range: 4.5V to 60V
- 1.5% Output Voltage Accuracy:  $1.2V \leq VOUT < 60V$
- 6% Output Current Accuracy:  $3V \leq VOUT < 60V$
- Input and Output Current Regulation with Current Monitor Outputs
- No Top FET Refresh in Buck or Boost
- VOUT Disconnected from VIN During Shutdown
- C/10 Charge Termination and Output Shorted Flags
- 38-Lead TSSOP with Exposed Pad

### APPLICATIONS

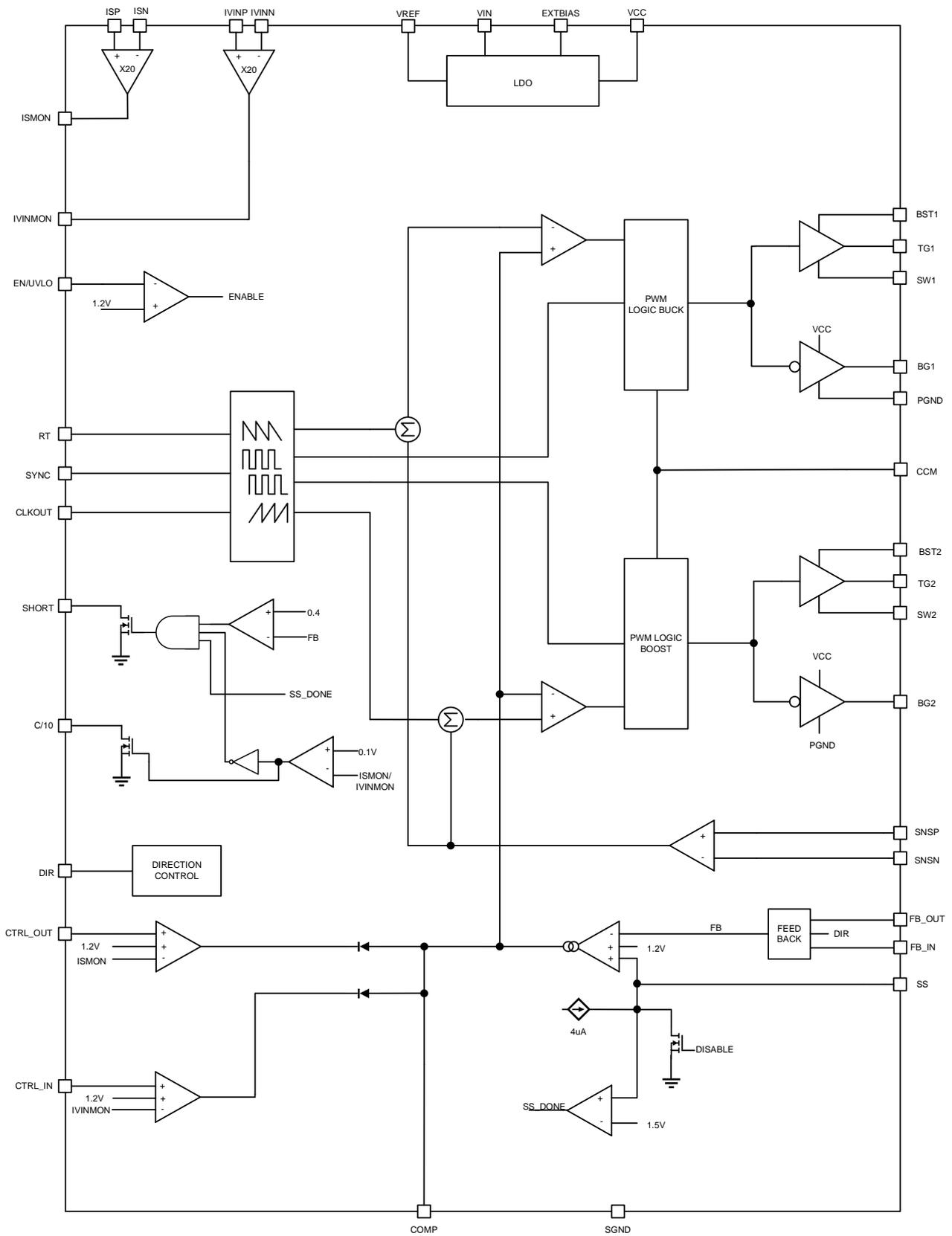
- Automotive, Telecom, Industrial Systems
- High Power Battery-Powered System
- Bidirectional Charging System
- Energy Store System
- High Power Battery-Powered System

TYPICAL APPLICATION



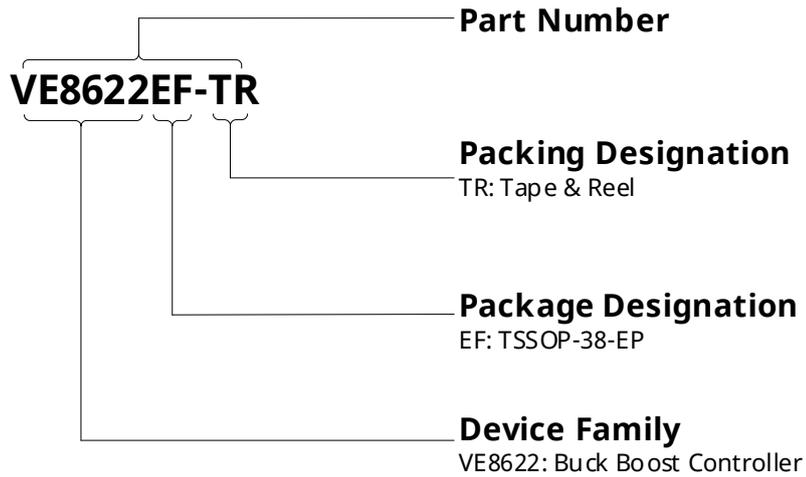
Bidirectional Application

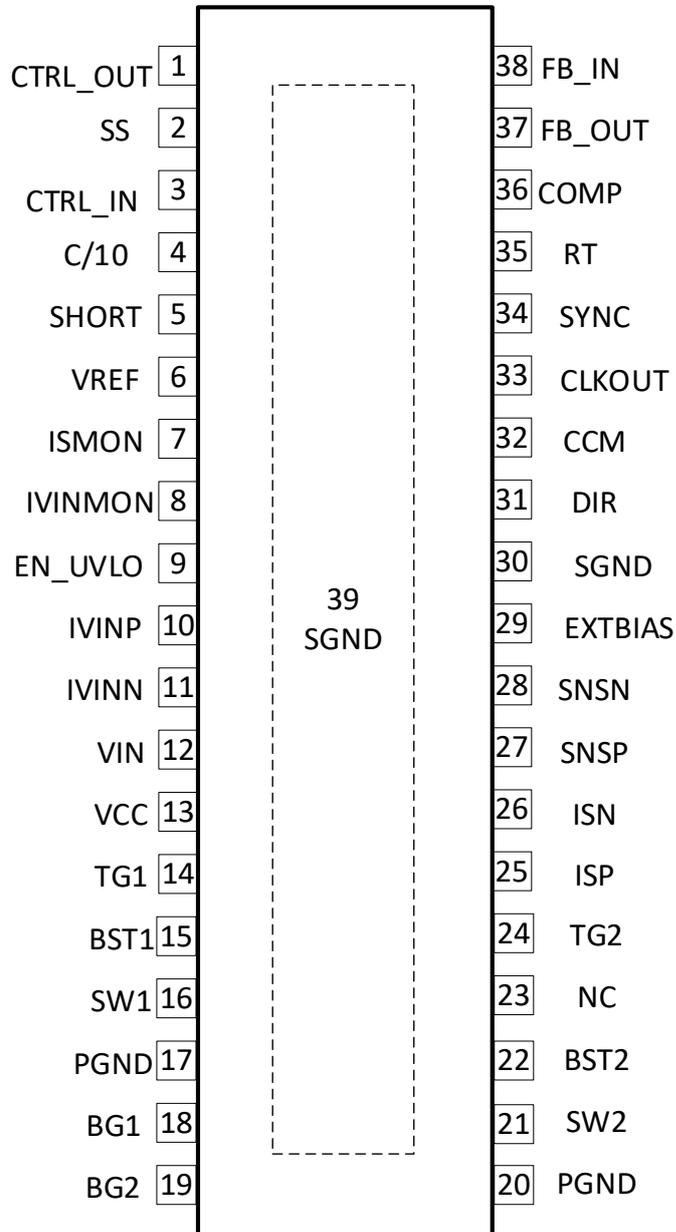
**BLOCK DIAGRAM**



**ORDERING INFORMATION**

Ordering Information	Mark	Temperature Range	Package	Pack	Quantity
VE8622EF-TR	8622	-40 to +125°C	TSSOP-38-EP	TR	4000



**PIN CONFIGURATIONS**


**PIN DESCRIPTION**

Pin	Name	Description
1	CTRL_OUT	Current Sense Threshold Adjustment Pin. Regulating threshold $V_{(ISP-ISN)}$ is 1/20th of $V_{CTRL\_OUT}$ . CTRL_OUT linear range is from 0V to 1.1V. For $V_{CTRL\_OUT} > 1.4V$ , the current sense threshold is constant at the full-scale value of 60mV. Connect CTRL_OUT to VREF for the 60mV default threshold. Force less than 50mV (typical) to stop switching. Do not leave this pin open.
2	SS	A regulated 4uA current charges up the SS capacitor. The value of this SS capacitor sets the output voltage ramp.
3	CTRL_IN	Current Sense Threshold Adjustment Pin. Regulating threshold $V_{(IVINP-IVINN)}$ is 1/20th of $V_{CTRL\_IN}$ . CTRL_IN linear range is from 0V to 1.1V. For $V_{CTRL\_IN} > 1.4V$ , the current sense threshold is constant at the full-scale value of 60mV. Connect CTRL_IN to VREF for the 60mV default threshold. Force less than 50mV (typical) to stop switching. Do not leave this pin open.
4	C/10	C/10 Charge Termination Pin. An open-drain pull-down on C/10 asserts if $V_{ISMON}(DIR=H)$ or $V_{IVINMON}(DIR=L)$ is less than 100mV (typical). To function, the pin requires an external pull-up resistor.
5	SHORT	Output Shorted Pin. An open-drain pull-down on SHORT asserts if $V_{FB\_OUT}(DIR=H)$ or $V_{FB\_IN}(DIR=L)$ is less than 400mV (typical) and $V_{ISMON}(DIR=H)$ or $V_{IVINMON}(DIR=L)$ is larger than 120mV (typical). To function, the pin requires an external pull-up resistor.
6	VREF	Voltage Reference Output Pin, typically 2V. Can supply up to 2mA of current.
7	ISMON	Monitor pin that produces a voltage that is twenty times the voltage $V_{(ISP-ISN)}$ . ISMON will equal 1.2V when $V_{(ISP-ISN)} = 60mV$ .
8	IVINMON	Monitor pin that produces a voltage that is twenty times the voltage $V_{(IVINP-IVINN)}$ . IVINMON will equal 1.2V when $V_{(IVINP-IVINN)} = 60mV$ .
9	EN_UVLO	Enable Control Pin. Forcing an accurate 1.2V rising threshold with 125mV hysteresis. An undervoltage condition resets soft-start. Tie to 0.3V, or less, to disable the device.
10	IVINP	Positive Input for the Input Current Limit and Monitor. Input bias current for this pin is typically 270μA.
11	IVINN	Negative Input for the Input Current Limit and Monitor.
12	VIN	Main Input Supply. Bypass this pin to PGND with a capacitor.
13	VCC	Internal 5V Regulator Output. The driver and control circuits are powered from this voltage. Bypass this pin to PGND with a minimum 4.7μF ceramic capacitor.
14	TG1	Top Gate Drive. Drives the top N-channel MOSFET.
15	BST1	Bootstrapped Driver Supply. Connect a bypass capacitor between BST1 and SW1. A Schottky or high-speed diode must be tied from VCC to BST1.
16	SW1	Switch Node.
17,20	PGND	Power Ground.
18	BG1	Bottom Gate Drive. Drives the gate of the bottom N-channel MOSFET between ground and VCC.
19	BG2	Bottom Gate Drive. Drives the gate of the bottom N-channel MOSFET

Pin	Name	Description
		between ground and VCC.
21	SW2	Switch Node.
22	BST2	Bootstrapped Driver Supply. Connect a bypass capacitor between BST2 and SW2.A Schottky or high-speed diode must be tied from VCC to BST2.
23	NC	No Connect Pin. Leave this pin floating.
24	TG2	Top Gate Drive. Drives the top N-channel MOSFET.
25	ISP	Connection Point for the Positive Terminal of the Output Current Feedback Resistor. Input bias current for this pin is typically 270 $\mu$ A.
26	ISN	Connection Point for the Negative Terminal of the Output Current Feedback Resistor.
27	SNSP	The Positive Input to the Current Sense Comparator.
28	SNSN	The Negative Input to the Current Sense Comparator.
29	EXTBIAS	External bias input for the optional VCC LDO. There is an internal switch to disconnect the VIN LDO when EXTBIAS voltage is higher than 4.7V. Decouple this pin to ground with a $\geq 1\mu$ F ceramic capacitor when it is in use. Connect this pin to ground if it is not used.
30	SNGD	Signal Ground. All small-signal components and compensation should connect to this ground, which should be connected to PGND at a single point. Solder the exposed pad directly to the ground plane.
31	DIR	Direction pin. When the pin voltage is higher than 1.5V(DIR=H), the part runs in forward operation. When the pin voltage is less than 0.3V(DIR=L), the part runs in reverse operation.
32	CCM	Continuous Conduction Mode Pin. When the pin voltage is higher than 1.5V, the part runs in fixed frequency forced continuous conduction mode and allows the inductor current to flow negative. When the pin voltage is less than 0.3V, the part runs in discontinuous conduction mode and does not allow the inductor current to flow backward. This pin is only meant to block inductor reverse current, and should only be pulled low when the output current is low. This pin must be either connected to VCC for continuous conduction mode across all loads, or it must be connected to the C/10 with a pull-up resistor to VCC for continuous conduction mode at heavy load and for discontinuous conduction mode at light load.
33	CLKOUT	Clock Output Pin. A 180° out-of-phase clock is provided at the oscillator frequency to allow for paralleling two devices for extending output power capability.
34	SYNC	External Synchronization Input Pin. The internal buck clock is synchronized to the rising edge of the SYNC signal while the internal boost clock is 180° phase shifted.
35	RT	Frequency Set Pin. Place a resistor to GND to set the internal frequency. The range of oscillation is 100kHz to 700kHz.
36	COMP	Current Control Threshold and Error Amplifier Compensation Point. The current comparator threshold increases with this control voltage.
37	FB_OUT	Voltage Loop Feedback Pin (DIR=H). FB_OUT is intended for constant-voltage regulation when the voltage of DIR is higher than 1.5V. The internal transconductance amplifier with output COMP will regulate FB_OUT to 1.2V

Pin	Name	Description
		through the DC/DC converter.
38	FB_IN	Voltage Loop Feedback Pin (DIR=L). FB_IN is intended for constant-voltage regulation when the voltage of DIR is less than 0.3V. The internal transconductance amplifier with output COMP will regulate FB_IN to 1.2V through the DC/DC converter.
39	Exposed Pad	Signal Ground. Solder the exposed pad directly to the ground plane.

**ABSOLUTE MAXIMUM RATINGS**

Parameter	Minimum	Maximum	Unit
VIN	-0.3	+75	V
EXTBIAS	-0.3	+26	
SW1, SW2	-0.3(-5V 20ns)	+75	V
C/10, SHORT	-0.3	+15	V
EN/UVLO, IVINP, IVINN, ISP, ISN	-0.3	+75	V
VCC, BST1-SW1, BST2-SW2	-0.3	+6.5	V
IVINP-IVINN, ISP-ISN, SNSP-SNSN	-0.3	+0.3	V
SNSP, SNSN	-0.3	+0.3	V
Other Pins	-0.3	+6.5	V
Storage Temperature	-65	+150	°C

**RECOMMENDED OPERATING CONDITIONS**

Parameter	Minimum	Maximum	Unit
VIN	+4.5	+60	V
EXTBIAS	+4.7	+24	V
VOUT	+1.2	+60	V
Operating Junction Temperature	-40	+125	°C

**THERMAL INFORMATION**

Thermal Resistance	$\theta_{JA}$ (°C/W)	$\theta_{JC}$ (°C/W)
TSSOP38	28	2

## ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified operating junction temperature range, otherwise specifications are at  $T_A = 25^\circ\text{C}$ ,  $V_{IN} = 12\text{V}$ , unless otherwise noted.

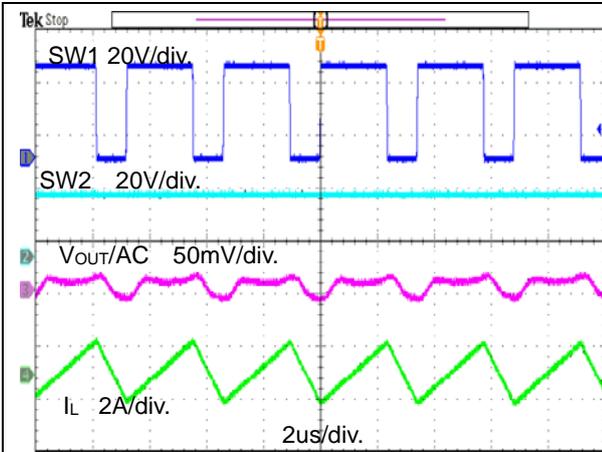
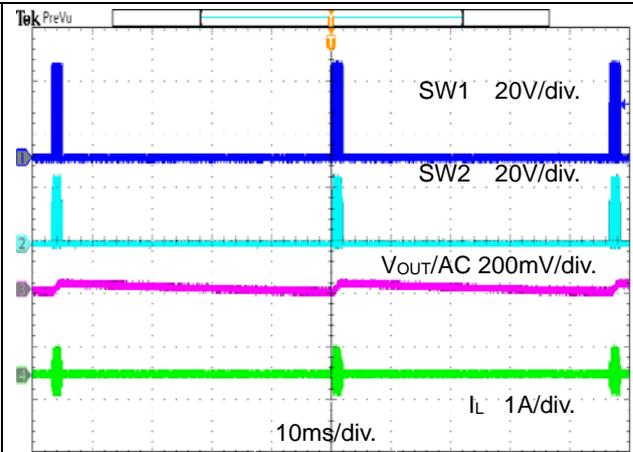
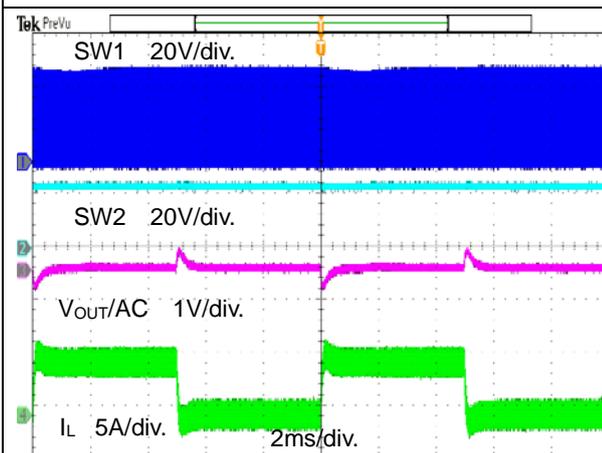
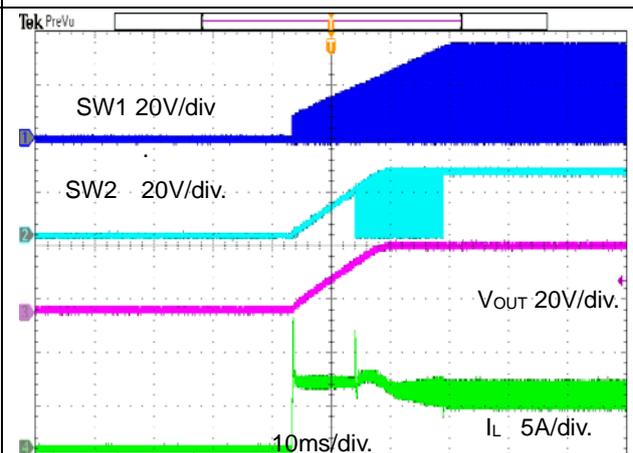
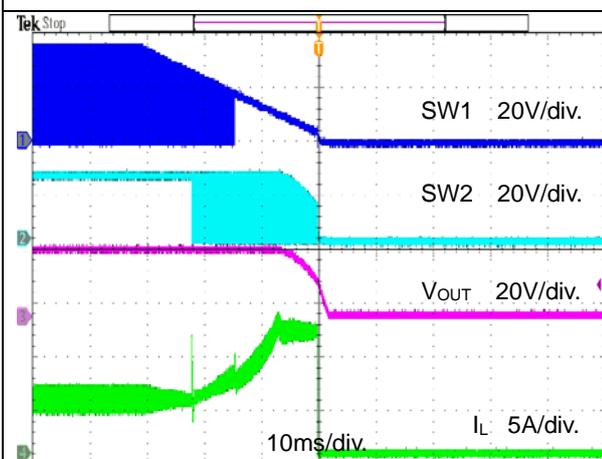
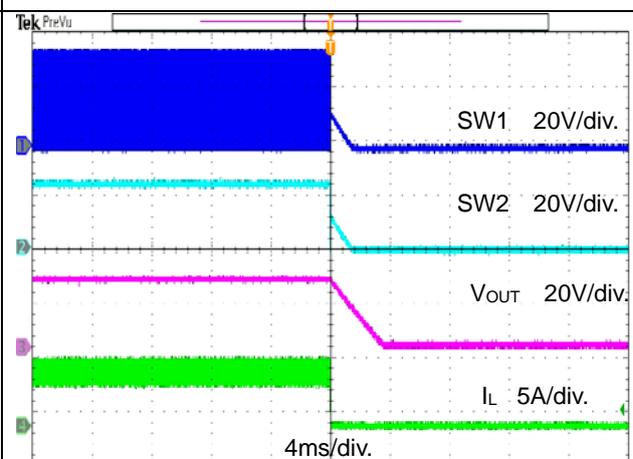
Parameter	Symbol	Test Condition	Min	Typ	Max	Unit
<b>Input</b>						
$V_{IN}$ Operating Voltage	$V_{IN}$		●	4.5	60	V
$V_{IN}$ Shutdown $I_Q$	$I_{shut}$	$V_{EN/UVLO} = 0\text{V}$		2		$\mu\text{A}$
$V_{IN}$ Operating $I_Q$ (Not Switching)	$I_Q$	$\text{FB} = 1.3\text{V}$ , $\text{RT} = 90\text{k}$		3		$\text{mA}$
<b>Logic Inputs</b>						
EN/UVLO Rising Threshold	$V_{EN}$		●	1.2		V
EN/UVLO Hysteresis			●	120		mV
EN/UVLO Pin Bias Current High		$V_{EN/UVLO} = 2\text{V}$		1		$\mu\text{A}$
CCM Threshold Voltage				0.3	1.5	V
CTRL Input Bias Current		$V_{CTRL} = 1\text{V}$		1		nA
CTRL Latch-Off Threshold		Rising		50		mV
CTRL Latch-Off Hysteresis				13		mV
<b>Regulation</b>						
VREF Voltage			●	2		V
$V_{(ISP-ISN)}$ Threshold	$V_{ISMON}$	$V_{CTRL\_OUT} = 2\text{V}$ , $V_{ISP} = 12\text{V}$	●	60		mV
		$V_{CTRL\_OUT} = 2\text{V}$ , $V_{ISP} = 1\text{V}$		60		mV
		$V_{CTRL\_OUT} = 1\text{V}$ , $V_{ISP} = 12\text{V}$	●	50		mV
		$V_{CTRL\_OUT} = 1\text{V}$ , $V_{ISP} = 1\text{V}$		50		mV
		$V_{CTRL\_OUT} = 0.6\text{V}$ , $V_{ISP} = 12\text{V}$	●	30		mV
		$V_{CTRL\_OUT} = 0.6\text{V}$ , $V_{ISP} = 1\text{V}$		30		mV
		$V_{CTRL\_OUT} = 0.1\text{V}$ , $V_{ISP} = 12\text{V}$	●	5		mV
		$V_{CTRL\_OUT} = 0.1\text{V}$ ,		5		mV

Parameter	Symbol	Test Condition	Min	Typ	Max	Unit
		$V_{ISP} = 1V$				
ISP Bias Current		$V_{ISP} = V_{ISN} = 12V$		270		$\mu A$
ISN Bias Current		$V_{ISP} = V_{ISN} = 12V$		1		$\mu A$
Output Current Sense Common Mode Range			0		60	V
ISMON Current Sense Amplifier gm				250		$\mu S$
ISMON Monitor Voltage		$V_{ISP} = 12V,$ $V_{(ISP-ISN)} = 60mV$	•	1.2		V
		$V_{ISP} = 12V,$ $V_{(ISP-ISN)} = 0V$	•		50	mV
$V_{(IVINP-IVINN)}$ Threshold		$V_{CTRL\_IN} = 2V,$ $V_{IVINP} = 12V$	•	60		mV
		$V_{CTRL\_IN} = 2V,$ $V_{IVINP} = 1V$		60		mV
		$V_{CTRL\_IN} = 1V,$ $V_{IVINP} = 12V$	•	50		mV
		$V_{CTRL\_IN} = 1V,$ $V_{IVINP} = 1V$		50		mV
		$V_{CTRL\_IN} = 0.6V,$ $V_{IVINP} = 12V$	•	30		mV
		$V_{CTRL\_IN} = 0.6V,$ $V_{IVINP} = 1V$		30		mV
		$V_{CTRL\_IN} = 0.1V,$ $V_{IVINP} = 12V$	•	5		mV
		$V_{CTRL\_IN} = 0.1V,$ $V_{IVINP} = 1V$		5		mV
IVINP Bias Current		$V_{IVINP} = V_{IVINN} = 12V$		270		$\mu A$
IVINN Bias Current		$V_{IVINP} = V_{IVINN} = 12V$		1		$\mu A$
Input Current Sense Common Mode Range			0		60	V
Input Current Sense Amplifier gm				250		$\mu S$
IVINMON Monitor Voltage		$V_{IVINP} = 12V,$ $V_{(IVINP-IVINN)} = 60mV$	•	1.2		V

Parameter	Symbol	Test Condition	Min	Typ	Max	Unit	
		$V_{IVINP}=12V$ , $V_{(IVINP-IVINN)} = 0V$	•	30		mV	
FB Regulation Voltage			•	1.2		V	
FB Amplifier gm				500		$\mu S$	
FB Pin Input Bias Current		FB in Regulation			100	nA	
$V_{SENSE(MAX)} (V_{SNSP}-V_{SNSN})$		Boost	•	46	55	60	mV
		Buck	•	-50	-40	-30	mV
<b>Soft Start</b>							
SS Pull-Up Current		$V_{SS} = 0V$		4		$\mu A$	
<b>Fault</b>							
C/10 Falling Threshold ( $V_{ISMON}$ )		$V_{ISP}=V_{ISN}=12V$		100		mV	
C/10 Falling Threshold ( $V_{IVINMON}$ )		$V_{IVINP}=V_{IVINN}=12V$		100		mV	
SHORT Falling Threshold ( $V_{FB\_OUT}$ OR $V_{FB\_IN}$ )				400		mV	
C/10 Pin Output Impedance				0.2		k $\Omega$	
SHORT Pin Output Impedance				0.2		k $\Omega$	
<b>Oscillator</b>							
Switching Frequency		$R_T = 90k$		500		kHz	
		MAX		700		kHz	
		MIN			100	kHz	
SYNC Frequency			150		700	kHz	
SYNC Threshold Voltage			0.3		1.5	V	
<b>V<sub>CC</sub> Regulator</b>							
V <sub>CC</sub> Regulation Voltage		$I_{VCC}=0A$	•	5		V	
		$I_{VCC}=10mA$	•	5		V	
V <sub>CC</sub> Undervoltage Lockout				3.5		V	
V <sub>CC</sub> Current Limit		$V_{CC} = 4V$		67		mA	
V <sub>CC</sub> from EXTBIAS Regulation Voltage				5		V	
EXTBIAS UVLO threshold (rising)				4.68		V	
EXTBIAS UVLO threshold (falling)				4.42		V	
EXTBIAS current Limit				110		mA	
<b>DIR</b>							

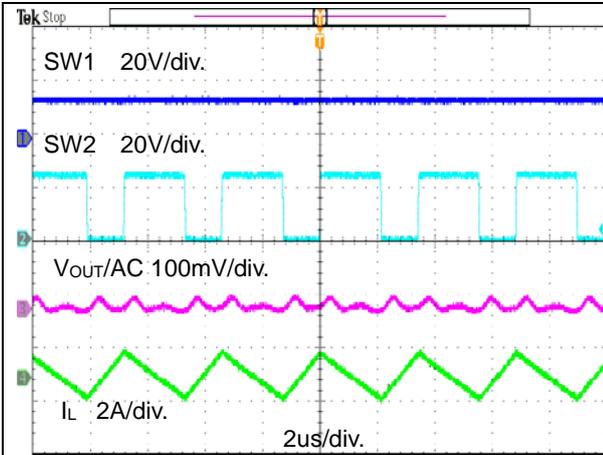
Parameter	Symbol	Test Condition	Min	Typ	Max	Unit
DIR Threshold Voltage			0.3		1.5	V
<b>Driver</b>						
TG1, TG2 Gate Driver On-Resistance		Gate Pull-Up, $V_{BST} - V_{SW} = 5V$		2		$\Omega$
		Gate Pull-Down, $V_{BST} - V_{SW} = 5V$		1		$\Omega$
BG1, BG2 Gate Driver On-Resistance		Gate Pull-Up, $V_{BST} - V_{SW} = 5V$		2		
		Gate Pull-Down, $V_{BST} - V_{SW} = 5V$		1		$\Omega$
TG1, TG2, $t_{OFF(MIN)}$		$R_T = 90k$		200		ns

**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

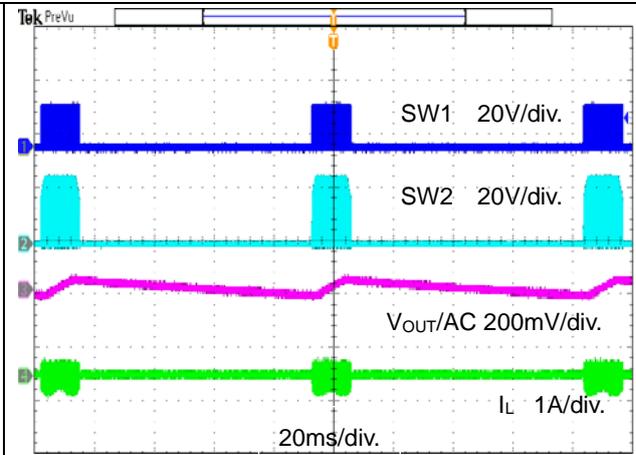
**TYPICAL PERFORMANCE CHARACTERISTICS**
 $V_{IN} = 35V$ ,  $V_{OUT} = 24V$ ,  $F_{sw} = 300\text{ kHz}$ ,  $T_J = -40^\circ\text{C}$  to  $+125^\circ\text{C}$ , unless otherwise noted.

**Figure 1. Steady State  $I_{OUT}=0A$  CCM**

**Figure 2. Steady State  $I_{OUT}=0A$  DEM**

**Figure 3. Dynamic Load  $I_{OUT}=0-5A$  CCM**

**Figure 4. Start Up  $I_{OUT}=5A$  CCM**

**Figure 5. Shut Down Through  $V_{IN}$   $I_{OUT}=5A$** 

**Figure 6. Shut Down Through  $EN$   $I_{OUT}=5A$**

**TYPICAL PERFORMANCE CHARACTERISTICS**

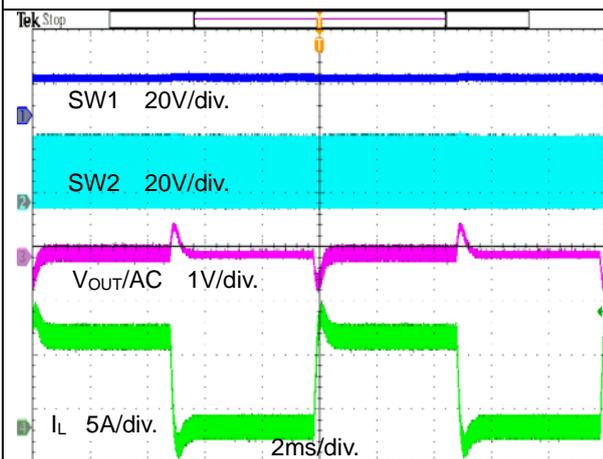
$V_{IN} = 15V$ ,  $V_{OUT} = 24V$ ,  $F_{sw} = 300\text{ kHz}$ ,  $T_J = -40^\circ\text{C}$  to  $+125^\circ\text{C}$ , unless otherwise noted.



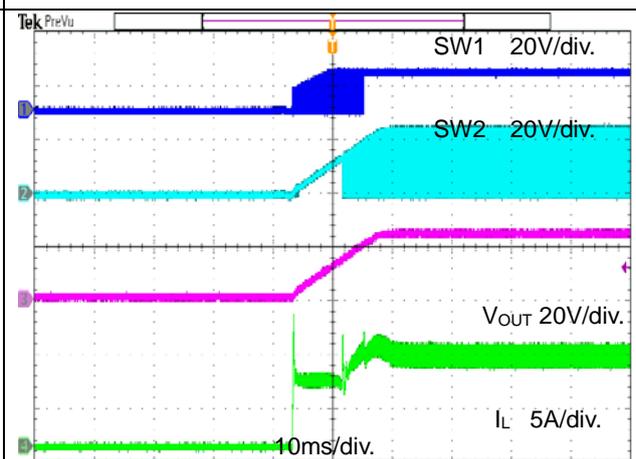
**Figure 7. Steady State  $I_{OUT}=0A$  CCM**



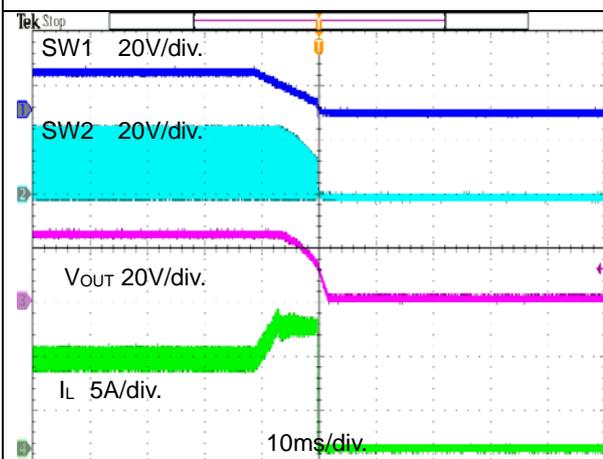
**Figure 8. Steady State  $I_{OUT}=0A$  DEM**



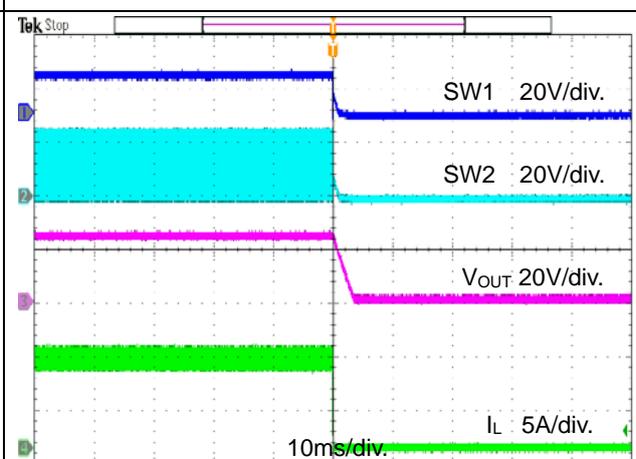
**Figure 9. Dynamic Load  $I_{OUT}=0-5A$  CCM**



**Figure 10. Start Up  $I_{OUT}=5A$  CCM**



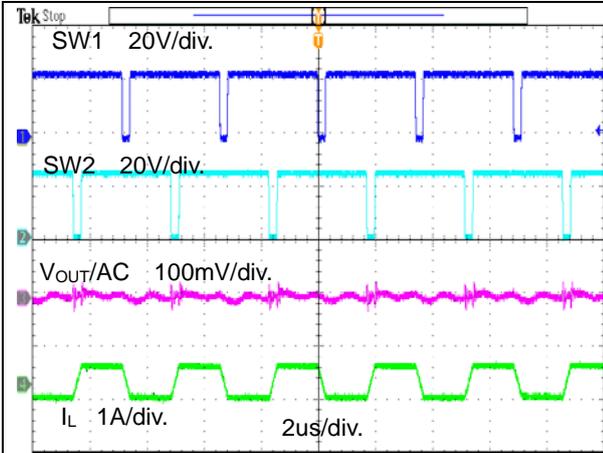
**Figure 11. Shut Down Through  $V_{IN}$   $I_{OUT}=5A$**



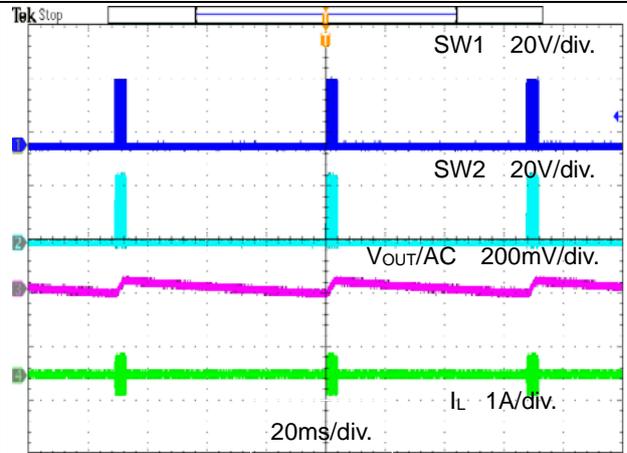
**Figure 12. Shut Down Through  $EN$   $I_{OUT}=5A$**

**TYPICAL PERFORMANCE CHARACTERISTICS**

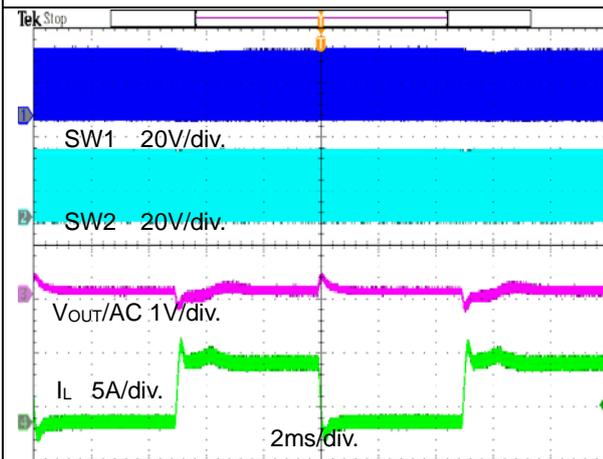
$V_{IN} = 24V$ ,  $V_{OUT} = 24V$ ,  $F_{sw} = 300\text{ kHz}$ ,  $T_J = -40^\circ\text{C}$  to  $+125^\circ\text{C}$ , unless otherwise noted.



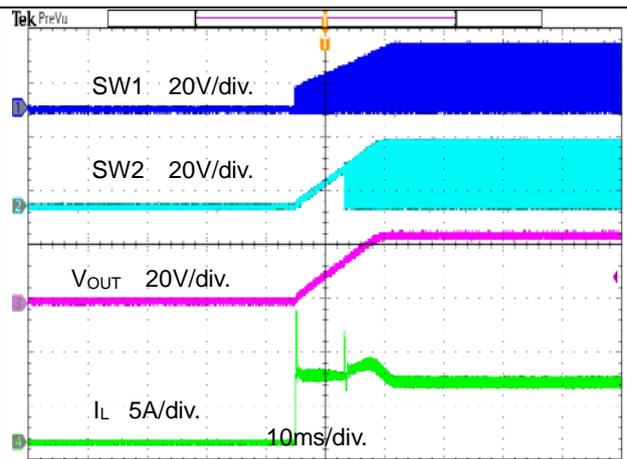
**Figure 13. Steady State  $I_{OUT}=0A$  CCM**



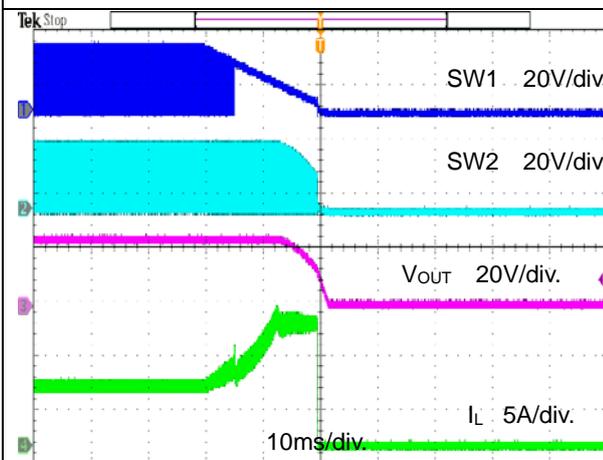
**Figure 14. Steady State  $I_{OUT}=0A$  DEM**



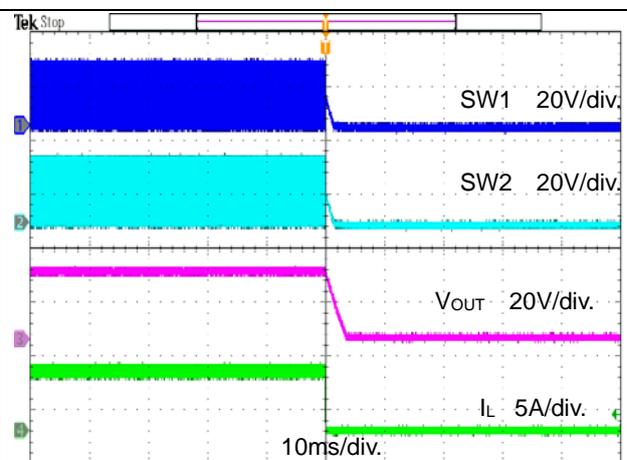
**Figure 15. Dynamic Load  $I_{OUT}=0-5A$  CCM**



**Figure 16. Start Up  $I_{OUT}=5A$  CCM**



**Figure 17. Shut Down Through  $V_{IN}$   $I_{OUT}=5A$**



**Figure 18. Shut Down Through  $EN$   $I_{OUT}=5A$**

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## FUNCTION DESCRIPTION

### Operation

The VE8622 is a current mode 4-switch buck-boost controller that provides an output voltage above, equal to or below the input voltage. The VE8622 uses current mode in buck or boost operation. It operates in buck mode when  $V_{IN}$  is greater than  $V_{OUT}$  and in boost mode when  $V_{IN}$  is less than  $V_{OUT}$ . It operates buck-boost mode when  $V_{IN}$  is close to  $V_{OUT}$ .

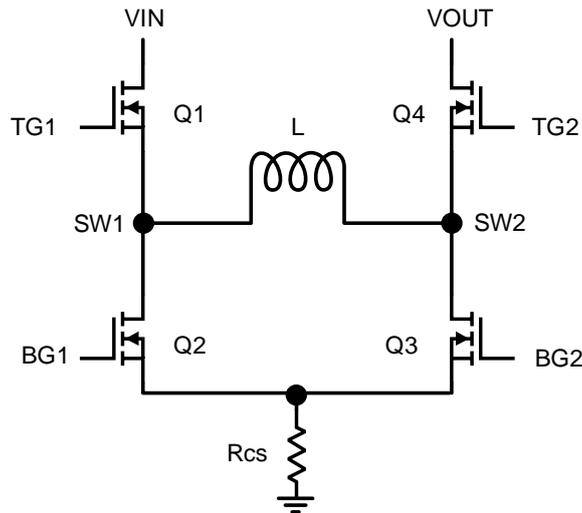


Figure 19. 4 Switch Buck-Boost

### Boost Mode

In boost mode switch Q1 is always on and switch Q2 is always off. It operates peak current mode boost as Figure 20, behaving like a typical synchronous boost regulator.

At the start of every cycle, switch Q3 is turned on first. Inductor current is sensed by Rcs when Q3 is turned on. After the sensed current exceeds the reference voltage, which is proportional to COMP, synchronous switch Q3 is turned off and switch Q4 is turned on for the remainder of the cycle.

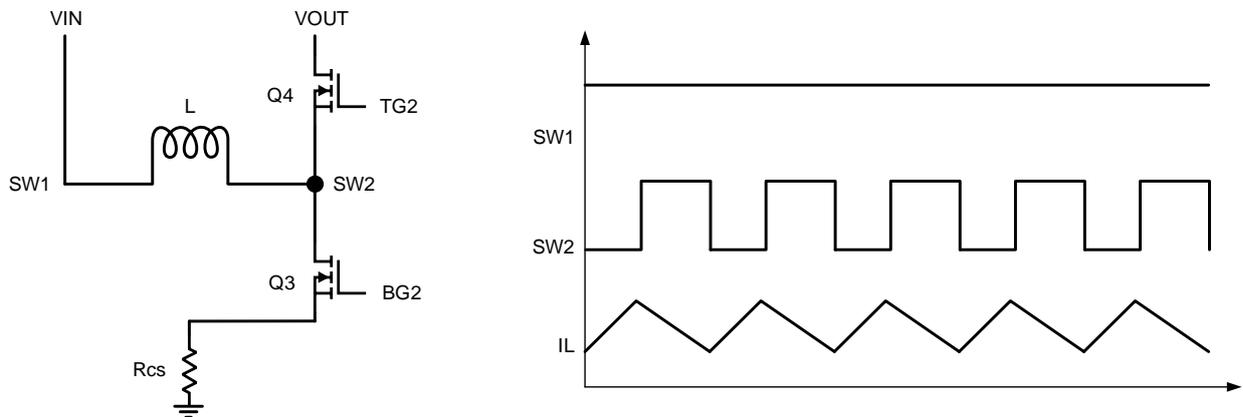


Figure 20. Boost Mode

### Buck Mode

In buck mode switch Q4 is always on and switch Q3 is always off. It operates valley current mode buck as Figure 21, behaving like a typical synchronous buck regulator.

At the start of every cycle, synchronous switch Q2 is turned on first. Inductor current is sensed by Rcs when Q2 is turned on. After the sensed current falls below the reference voltage, which is proportional to COMP, synchronous switch Q2 is turned off and switch Q1 is turned on for the remainder of the cycle.

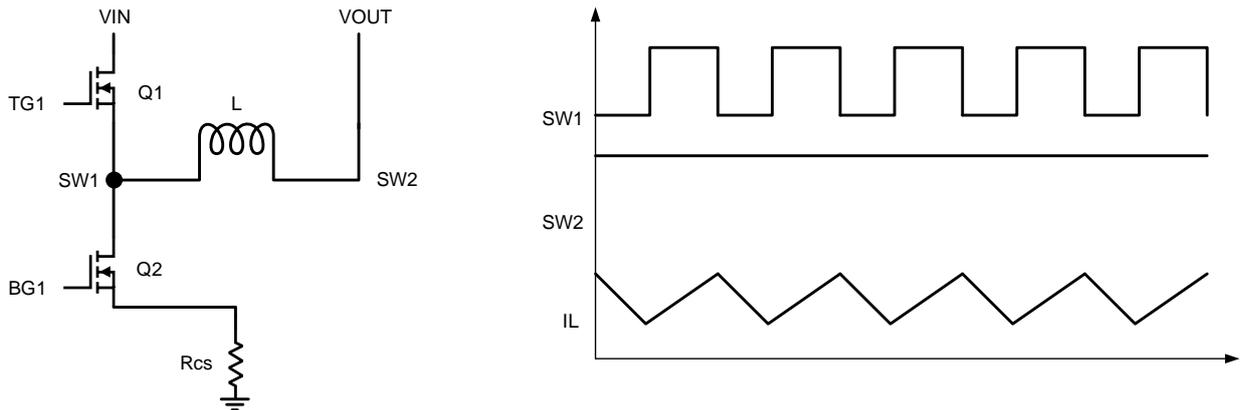


Figure 21. Buck Mode

### Buck-boost Mode

VE8622 works in buck-boost mode as Figure 22 when VIN approaches the VOUT. Every cycle VE8622 turns on switches Q2 and Q4, then Q1 and Q4 are turned on until 180° later when switches Q1 and Q3 turn on, and then switches Q1 and Q4 are turned on for the remainder of the cycle.

When VIN is higher than VOUT but close to VOUT,

The VE8622 enters the buck-boost mode when the duty cycle of buck  $D_{buck}$  is greater than

$$D_{bb1} = (T - 250\text{ns}) / T$$

Where T is the switching period.

$$D_{buck} = T_{on\_TG1} / T$$

It exits from buck-boost mode and return to buck mode when  $D_{buck}$  is less than

$$D_{bb2} = 1 - (0.25T + 200\text{ns}) / T$$

When VIN is lower than VOUT but close to VOUT,

The VE8622 enters the buck-boost mode when the duty cycle of boost  $D_{boost}$  is less than

$$D_{bb3} = 250\text{ns} / T$$

$$D_{boost} = T_{on\_BG2} / T$$

It exits from buck-boost mode and return to boost mode when  $D_{boost}$  is higher than

$$D_{bb4} = (0.25T + 200\text{ns}) / T.$$

Figure 23 shows operating mode vs duty cycle

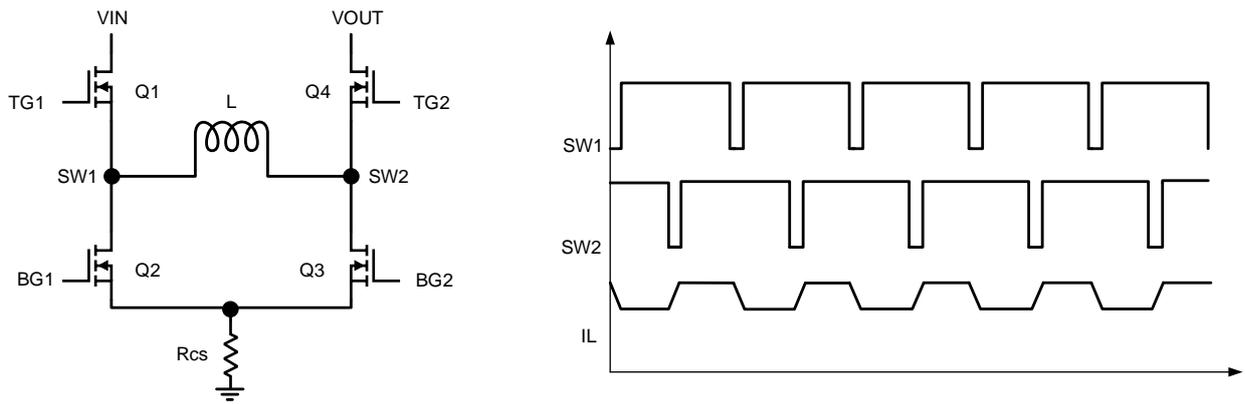


Figure 22. Buck-Boost Mode

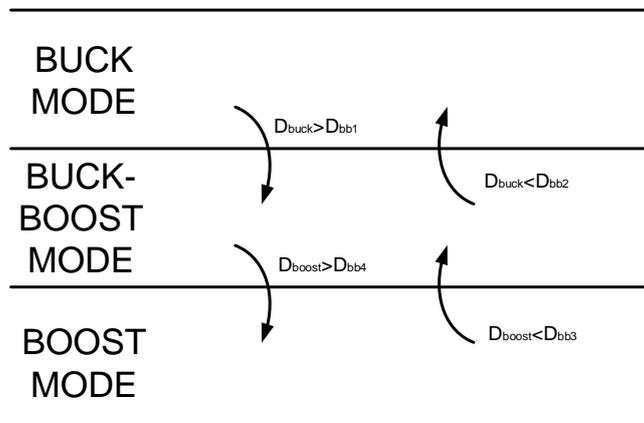


Figure 23. Mode vs Duty Cycle

**EN\_UVLO**

The VE8622 has a dedicated enable (EN\_UVLO) control that uses a bandgap - generated precision threshold of 1.2V. By pulling EN\_UVLO high or low, the IC can be enabled or disabled.

**VCC Regulator Connection**

VCC can be powered from both VIN and EXTBIAS. If connecting EXTBIAS to an external power supply, EXTBIAS should be higher than 4.7V but less than 24V. When VIN is less than 5.5V, EXTBIAS should be biased by external source. If VOUT is higher than 5V but less than 24V, EXTBIAS can be connected to VOUT with a resistor or diode. The recommend value of this resistor is 10Ω.

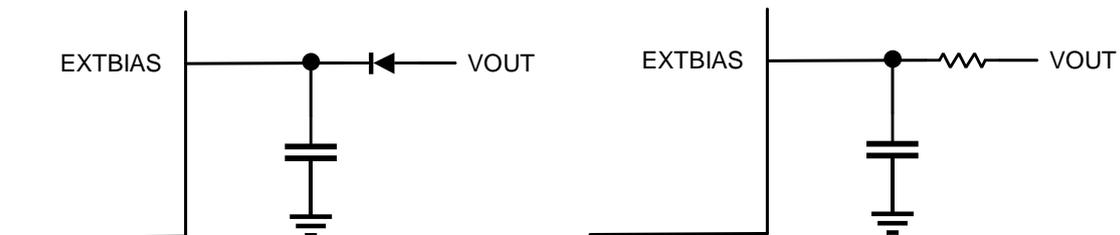


Figure 24. EXTBIAS Connection

### Low Current Operation

The VE8622 is recommended to run in forced continuous conduction mode at heavy load by pulling the CCM pin higher than 1.5V. In this mode the controller behaves as a continuous current mode synchronous switching regulator.

However, reverse inductor current from the output to the input is not desired for certain applications. For these applications, the CCM pin must be connected to GND. It also can be pulled low by the C/10 pin when the output current is low. In this mode, switch Q4(DIR=H) or Q1(DIR=L) turns off when the inductor current flows negative.

### Programming Frequency

The VE8622's frequency can be programmed from 100KHz to 700KHz with a resistor from RT to SGND. The Value of  $R_{RT}$  can be calculated with Equation (1):

$$R_{RT}(K\Omega) = \frac{1000}{0.0202 \times F_{SW}(KHz)} - 9 \quad (1)$$

### Frequency Synchronization

The VE8622 switching frequency can be synchronized from 150K to 700K using the SYNC pin. Driving SYNC with a pulse the duty cycle between 10% and 90%. The frequency of external clock must be higher than 70% of the frequency set by  $R_{RT}$ .

### Soft Start (SS)

Soft start (SS) is implemented to prevent the converter output voltage from overshooting during start-up. When the chip starts up, the internal circuitry generates a soft-start voltage that ramps up from 0V to 3V. When it is lower than REF, SS overrides REF, so the error amplifier uses SS as the reference. When SS is higher than REF, REF regains control.

An external capacitor connected from SS to SGND is charged from an internal 4 $\mu$ A current source, producing a ramped voltage. The soft - start time ( $T_{SS}$ ) is set by the external SS capacitor and can be calculated by Equation (2):

$$T_{SS}(ms) = \frac{C_{SS}(nF) \times V_{REF}(V)}{I_{SS}(\mu A)} \quad (2)$$

Where  $C_{SS}$  is the external SS capacitor,  $V_{REF}$  is the internal reference voltage (1.2V), and  $I_{SS}$  is the 4 $\mu$ A SS charge current. There is no internal SS capacitor. SS is reset when a fault protection occurs.

### SHORT Pin

The VE8622 provides an open-drain status pin, SHORT, which pulls low when the  $V_{FB\_OUT}$  pin is below 400mV and  $V_{ISMON}$  is above 120mV if VE8622 works in forward operation. It pulls low when the  $V_{FB\_IN}$  pin is below 400mV and  $V_{IVINMON}$  is above 120mV if VE8622 works in reverse operation. The only time the  $V_{FB\_OUT}$  or  $V_{FB\_IN}$  will be below 400mV is during start-up or if the output is shorted. During start-up the VE8622 ignores the voltage on the FB\_OUT or FB\_IN pin until the soft-start capacitor reaches 1.5V.

### C/10 Pin

The VE8622 provides an open-drain status pin, C/10, which pulls low when the voltage  $V_{ISMON}$  is less than 100mV if VE8622 works in forward mode. It pulls low when the voltage across  $V_{IVINMON}$  is less than 100mV if

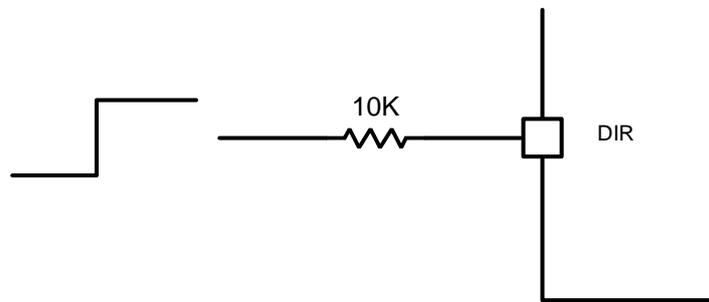
VE8622 works in reverse mode. For battery charger applications with output current sense and limit, the C/10 provides a C/10 charge termination flag.

### Gate Driver

The low-side gate driver is supplied from VCC. The high-side gate driver is supplied from BST. A boot capacitor connected from the BST to the SW provides power to the high-side MOSFET driver. This floating driver has its own under-voltage lockout (UVLO) protection. This UVLO's rising threshold is 3.6V with a hysteresis of 100mV. If the BST voltage is lower than the bootstrap UVLO, the VE8622 enters boot refresh mode to ensure that the BST capacitor is high enough to drive the HS-FET.

### Direction

Pulling high the DIR pin by a 10K resistor to set the mode as forward operation. Pulling low the DIR pin by a 10K resistor to set the mode as reverse operation.



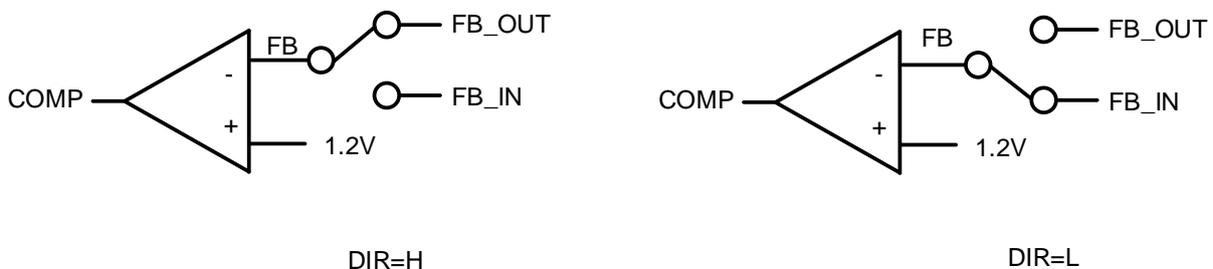
**Figure 25. DIR Connection**

**Table 1. DIR Vs Operation Mode**

DIR	Operation Mode
High	Forward
Low	Reverse

### Voltage Feedback

The FB\_IN or FB\_OUT is used to set the regulated voltage. FB\_OUT is used to set the regulated voltage when DIR is high and FB\_IN is used to set the regulated voltage when DIR is Low.



**Figure 26. Voltage Feedback**

Table 2. DIR Vs Feedback

DIR	FB_IN	FB_OUT
High	Idle	Active
Low	Active	Idle

**Current Monitor**

The VE8622 has two current sense operational amplifiers which can monitor both input and output current when it works in unidirectional mode.

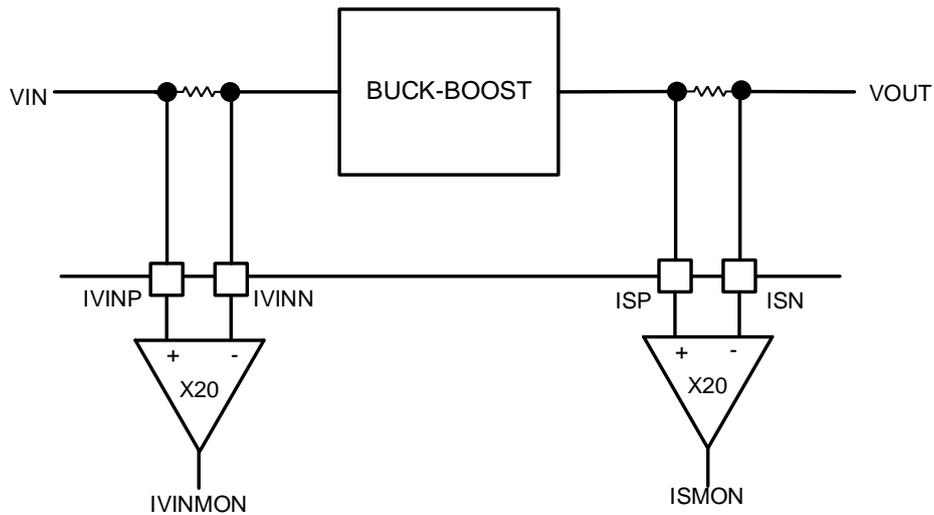
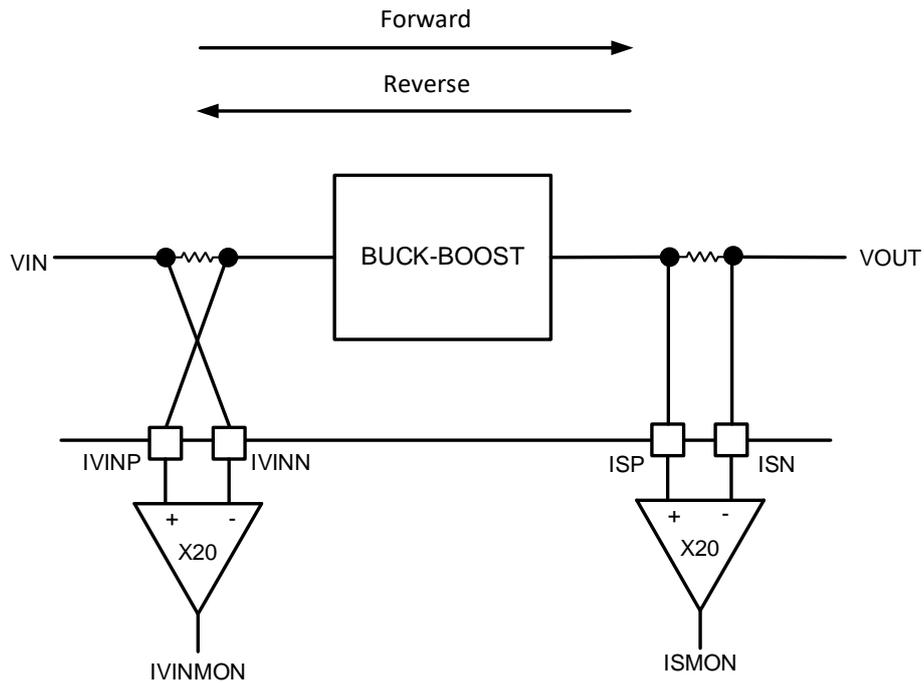


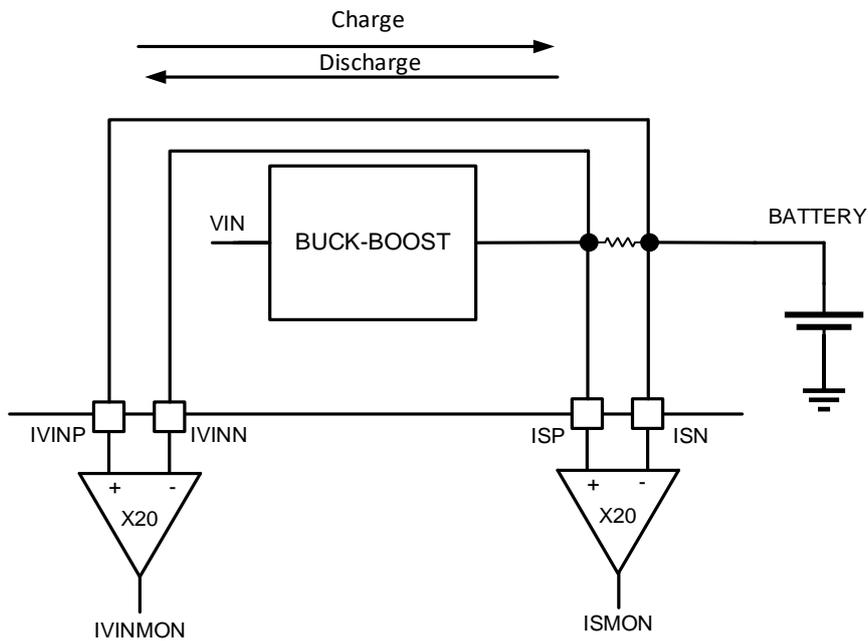
Figure 27. Input and Output Current Monitor

If VE8622 works in bidirectional mode, one of the amplifiers monitors the forward output current while another monitors the reverse output current.



**Figure 28. Bidirectional Current Monitor**

VE8622 can monitors both charging and discharging current when it works in battery charge/discharge mode.



**Figure 29. Battery Charge and Discharge Current Monitor**

**ISMON and IVINMON**

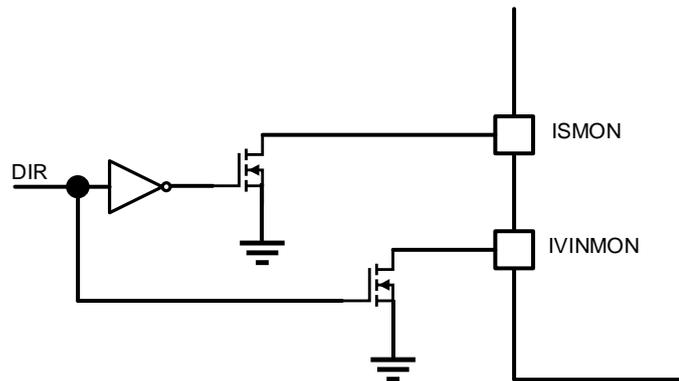
The ISMON and IVINMON pins provide a linear indication of the current flowing through the output. The equation for  $V_{ISMON}$  and  $V_{IVINMON}$  are

$$V_{ISMON} = 20 \times V_{(ISP-ISN)}$$

$$V_{IVINMON} = 20 \times V_{(IVINP-IVINN)}$$

These pins are suitable for driving an ADC input, however, the output impedance of these pins is 80kΩ so care must be taken not to load this pin.

To avoid wrong operation, ISMON or IVINMON must be pulled down when the VE8622 works in bidirectional mode or battery charging/ discharging mode. IVINMON must be pulled down when VE8622 works in forward operation, and ISMON must be pulled down when it works in reverse operation.



**Figure 30. ISMON and IVINMON Set Up for Bidirectional Mode**

**Table 3. DIR Vs Current Monitor**

DIR	IVINMON	ISMON
High	Pull low	Active
Low	Active	Pull low

**Current Control**

The CTRL\_OUT and CTRL\_IN can be used to adjust the current. When the CTRL\_OUT voltage is less than 1.1V, the voltage on the ISMON pin is limited to the voltage on the CTRL\_OUT pin. When the CTRL\_IN voltage is less than 1.1V, the voltage on the IVINMON pin is limited to the voltage on the CTRL\_IN pin.

When the CTRL\_OUT or CTRL\_IN pin voltage is between 1.1V and 1.4V the voltage on the ISMONT or IVINMON pin varies with VCTRL\_OUT or VCTRL\_IN. when VCTRL\_IN or VCTRL\_OUT > 1.4V the voltage on the ISMON or IVINMON pin no longer varies.

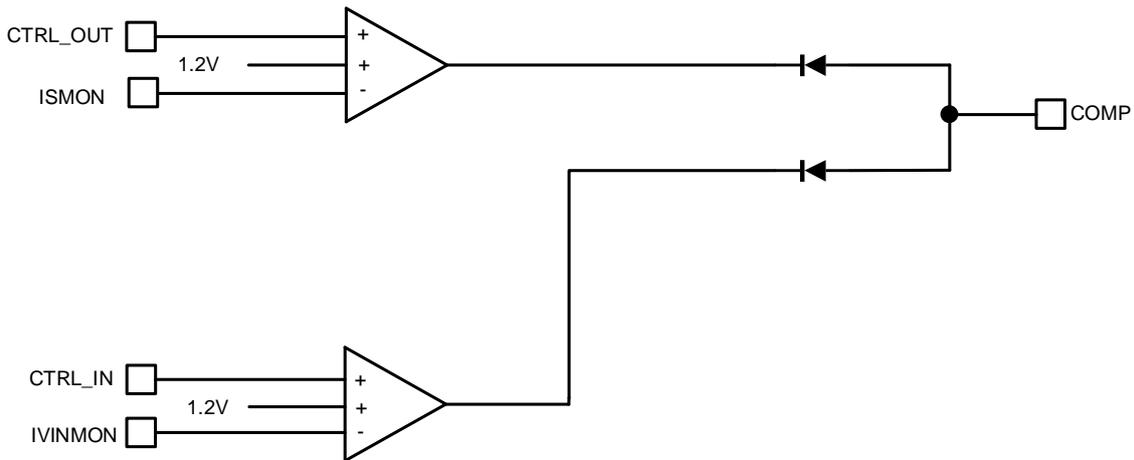


Figure 31. Current Control

**Low Side Current Sense**

The SNSP and SNSN pins sense the low side current which is used to implement the current mode control and peak valley current limit. To prevent false triggering due to the switching noise, an RC filter maybe required.

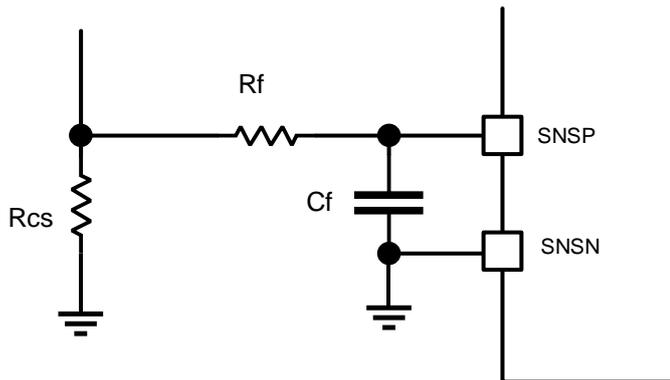


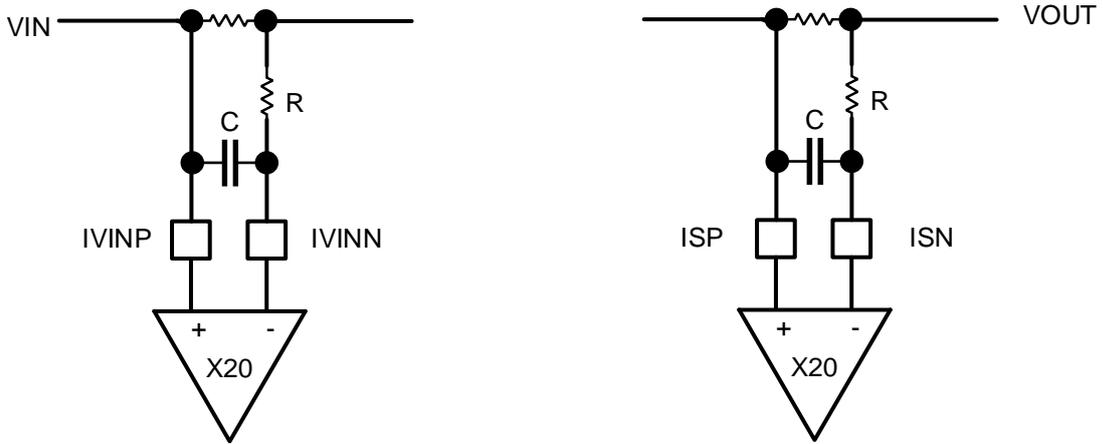
Figure 32. Filter for Low Side Current Sense

**Voltage Loop Compensation**

The compensation resistor and capacitor at COMP are set to optimize the voltage loop. The typical value of the compensation capacitor is 22n and the value of compensation resistor is 10k. Higher capacitance and lower resistance will improve stability but will slow the loop response.

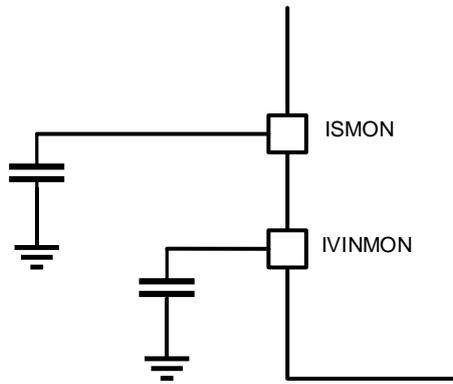
**Current Loop Compensation**

The filter of current sense will improve the stability of current loop. Connecting a RC filter to IVINN or ISN if the ripple current on the current sense resistor is large. Do not connect the resistor to IVINP or ISP pin.



**Figure 33. High Side Current Loop Compensation**

Another way to filter the current signal is connecting a capacitor to ISMON or IVINMON.



**Figure34. Low Side Current Loop Compensation**

## PCB Layout Guidelines

1. The PGND ground plane layer should not have any traces and it should be as close as possible to the layer with power MOSFETs.
2. Place  $C_{IN}$ , switch Q1, switch Q2 in one compact area. Place  $C_{OUT}$ , switch Q3, switch Q4 in one compact area.
3. Keep the high dv/dt SW1, SW2, BST1, BST2, TG1 and TG2 nodes away from sensitive small-signal nodes.
4. The path formed by switch Q1, switch Q2, and the  $C_{IN}$  capacitor should have short leads and PC trace lengths. The path formed by switch Q3, switch Q4, and the  $C_{OUT}$  capacitor also should have short leads and PC trace lengths.
5. Connect the top driver bootstrap capacitor, C1, closely to the BST1 and SW1 pins. Connect the top driver bootstrap capacitor, C2, closely to the BST2 and SW2 pins.
6. Connect the input capacitors,  $C_{IN}$ , and output capacitors,  $C_{OUT}$ , closely to the power MOSFETs. These capacitors carry the MOSFET AC current in boost and buck operation.
7. Route SNSN and SNSP leads together with minimum PC trace spacing. Avoid sense lines pass through noisy areas, such as switch nodes. Ensure accurate current sensing with Kelvin connections at the SENSE resistor.
8. Connect the COMP pin compensation network close to the IC, between COMP and the signal ground pins. The capacitor helps to filter the effects of PCB noise and output voltage ripple voltage from the compensation loop.
9. Connect the VCC bypass capacitor close to the IC, between the VCC and the power ground pins. This capacitor carries the MOSFET drivers' current peaks.

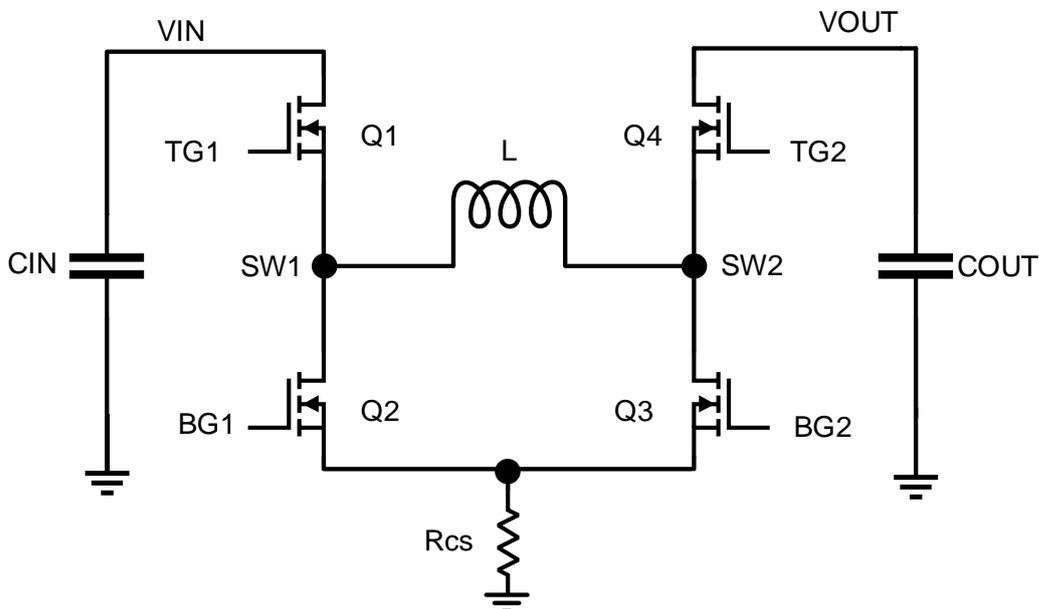
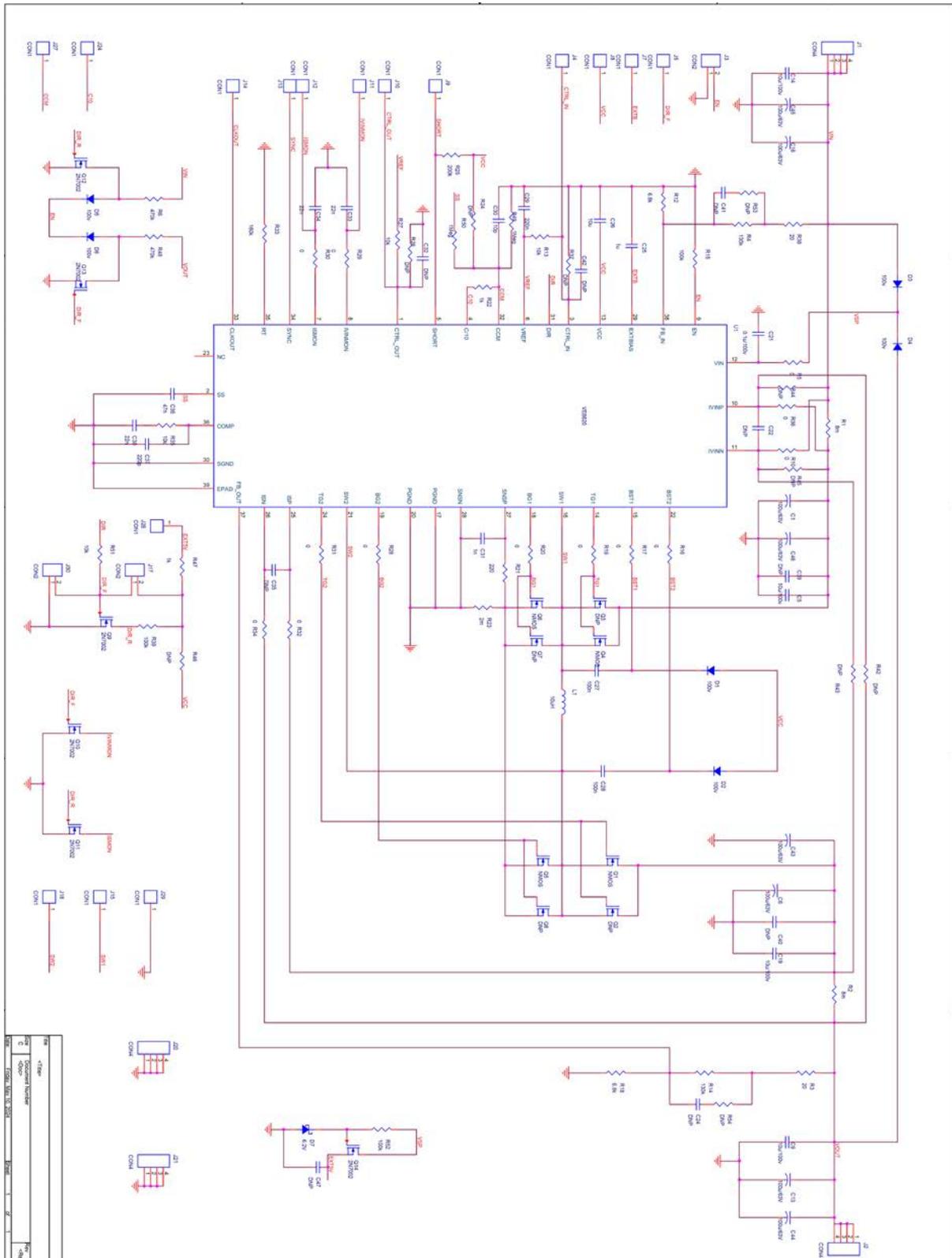
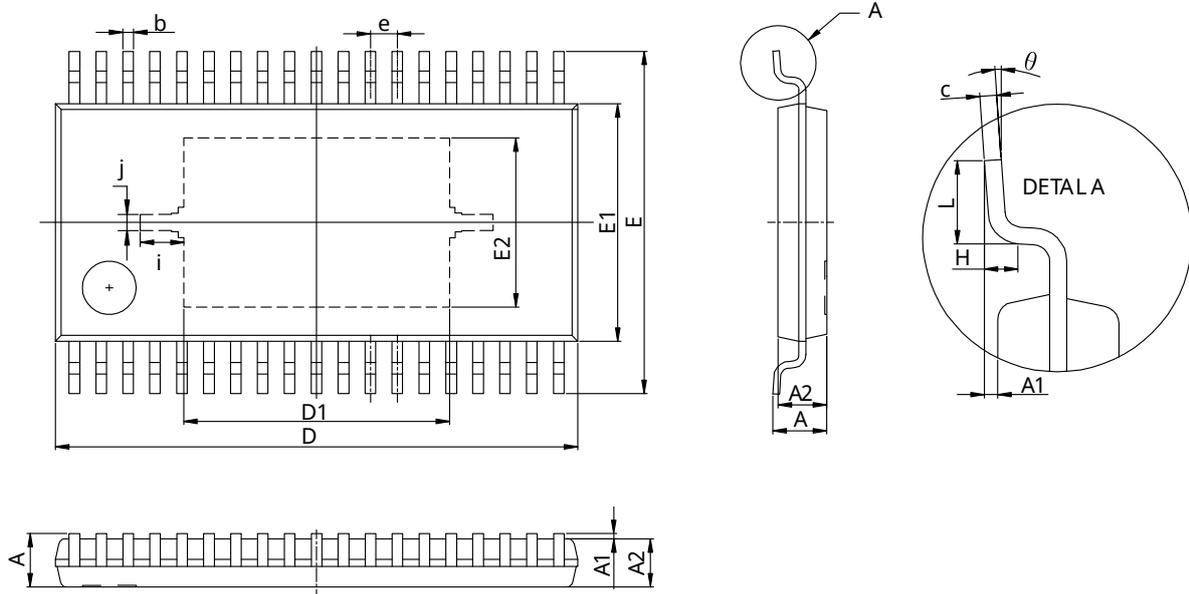


Figure 35. Power Stage of Buck-Boost

TYPICAL APPLICATION CIRCUIT



**PACKAGE INFORMATION**
**TSSOP-38-EP**


Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min.	Max.	Min.	Max.
A	-	1.200	-	0.047
A1	0.050	0.150	0.002	0.006
A2	0.800	1.000	0.031	0.039
b	0.170	0.270	0.007	0.011
c	0.090	0.200	0.004	0.008
D	9.600	9.800	0.378	0.386
D1	4.840	5.040	0.191	0.198
E	6.250	6.550	0.246	0.258
E1	4.300	4.500	0.169	0.177
E2	3.060	3.260	0.120	0.128
e	0.0500(BSC)		0.020(BSC)	
L	0.500	0.700	0.020	0.028
H	0.250(TYP)		0.010(TYP)	
i	0.705	0.905	0.028	0.036
j	0.200	0.400	0.008	0.016
θ	1°	7°	1°	7°

**REVISION HISTOR**

Revision	Data	Description
1.0	2024-10-15	Initial Release

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